

# NextGen Geothermal Power NGP makes CO<sub>2</sub> work!

Maturing Geothermal Energy for KSA

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- **CO<sub>2</sub>-based geothermal power generation**  
motivation, basic concept, technology description
- **thermodynamic evaluation**  
direct CO<sub>2</sub> cycle | indirect brine cycle  
sensitivities of geologic and ambient boundary conditions  
scaling of wellfield pattern
- **site analysis & turbine design**  
site selection, use cases, turbine blade path design
- **economic evaluation**  
assessment of spec. CAPEX and LCOE
- **summary & outlook**

# How to push renewables and carbon capture & storage to meet climate goals?



- the world is way off track in meeting the Paris Agreement climate goals
- wind & solar power has limited availability (not 24/7)
- geothermal power is fully dispatchable, but hydro-based applications are regionally restricted
- Carbon Capture & Storage (CCS) is essential to limit the global warming below 2 °C but :  
No value add and recognized as „disposal“

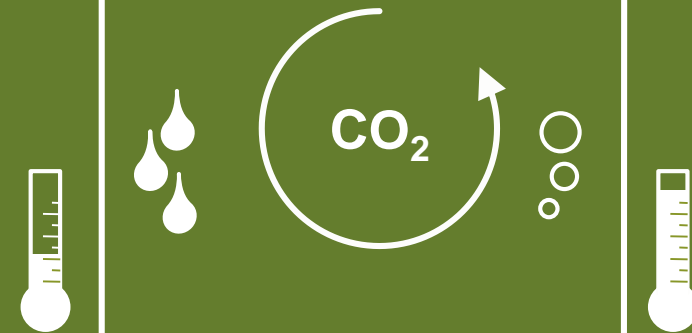


# Combination of geothermal energy with carbon capture & storage

**SIEMENS**  
*Ingenuity for life*

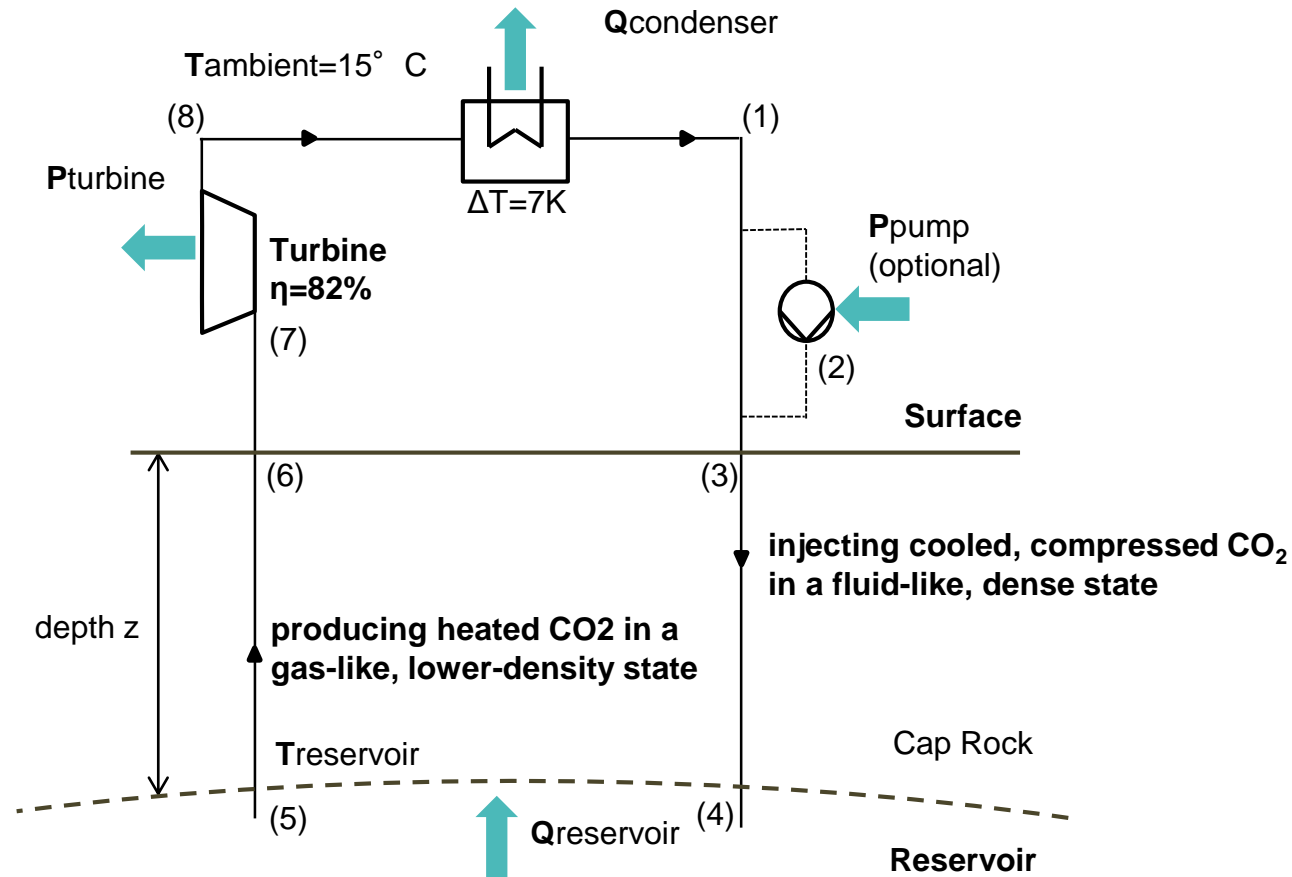


- NGP combines geothermal energy with CCS and transforms CCS to CCUS
- CO<sub>2</sub> is injected in sedimentary basins that host high-permeability reservoirs overlain by cap rocks
- heated by geothermal energy, CO<sub>2</sub> flows to the surface and expands in a turbine to generate electricity
- NGP creates valuable power that makes CCS comfortable

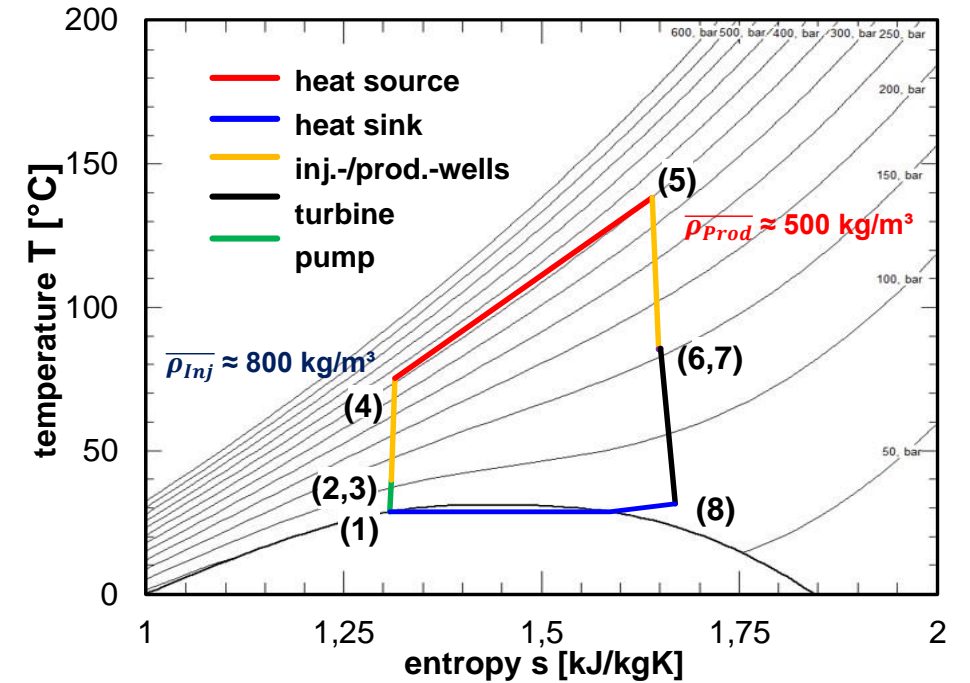


# Advantages of CO2 as a geothermal working medium

## thermosyphon effect



$$\Delta p_{reservoir} = \frac{\mu \cdot L}{\rho \cdot A} \cdot \frac{\dot{m}}{\kappa} = M \cdot \dot{m} \quad (\text{Darcy's law})$$

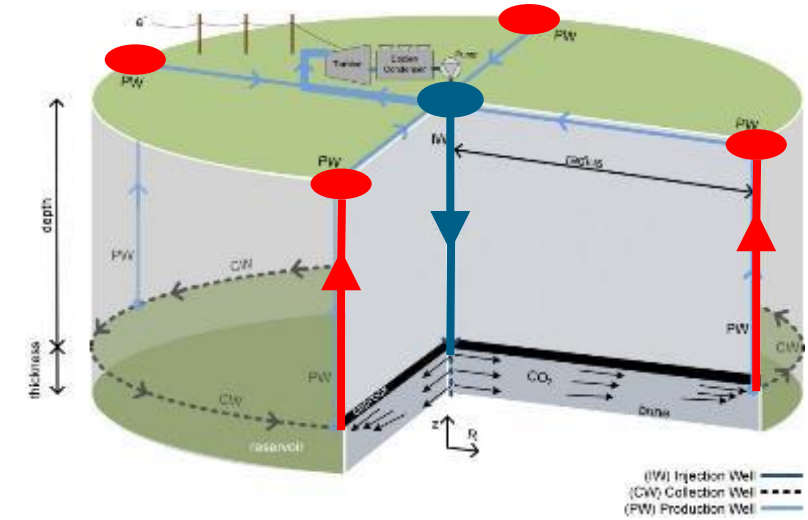


- due to the geothermal heat supply, a density difference between injection and production arises
- the pressure gradient along the wells is different in size and leads to a difference between the well heads
 
$$\Delta p_{TS} = (\bar{\rho}_{inj} - \bar{\rho}_{prod}) \cdot g \cdot \Delta z$$
- driven by the thermosyphon, pumping work is reduced

# Assessment of NGP Systems

## Geologic conditions – Base Case

Coordination number	1 (5-spot-system)
Depth	2500 m
Well diameter	0,41 m
Permeability-thickness product (kh)	15.000 mD·m
Temp. gradient	35 K/km



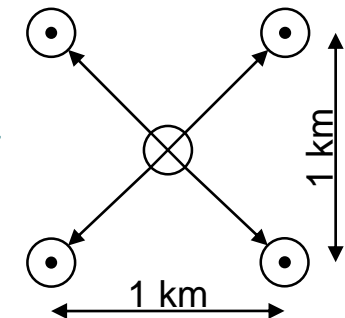
Saar, Adams; Subsurface Energy Storage with CO<sub>2</sub>; 2018

## Power Cycle Variants

direct   sCO <sub>2</sub>		indirect   Brine - Isobutane	
Thermosiphon only	with supplemental pumping	single pressure	dual pressure

### Base Case well pattern

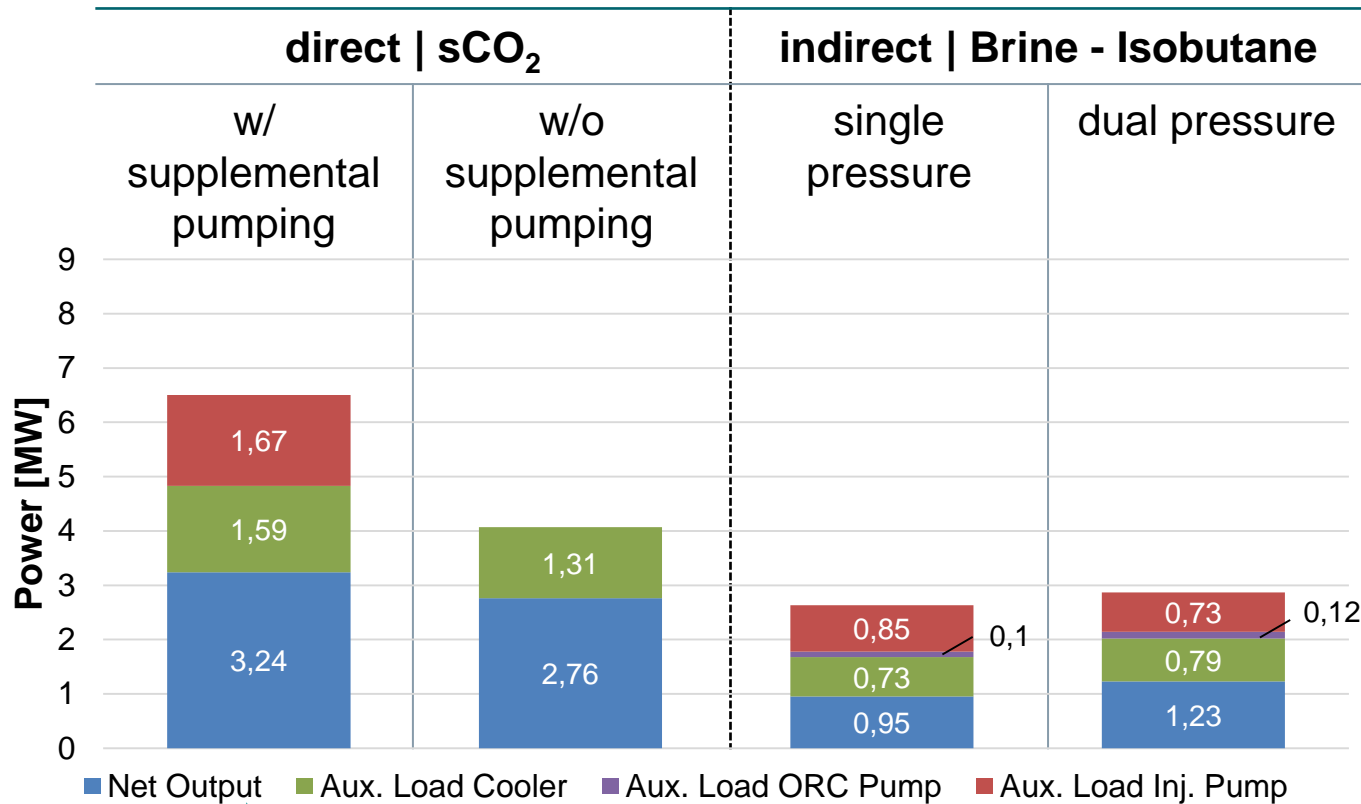
- ⊙ production well
- ⊗ injection well



# Calculation results for NGP base case



## Power Cycle Variants



x3,4  
x2,5

### Reservoir conditions: base case

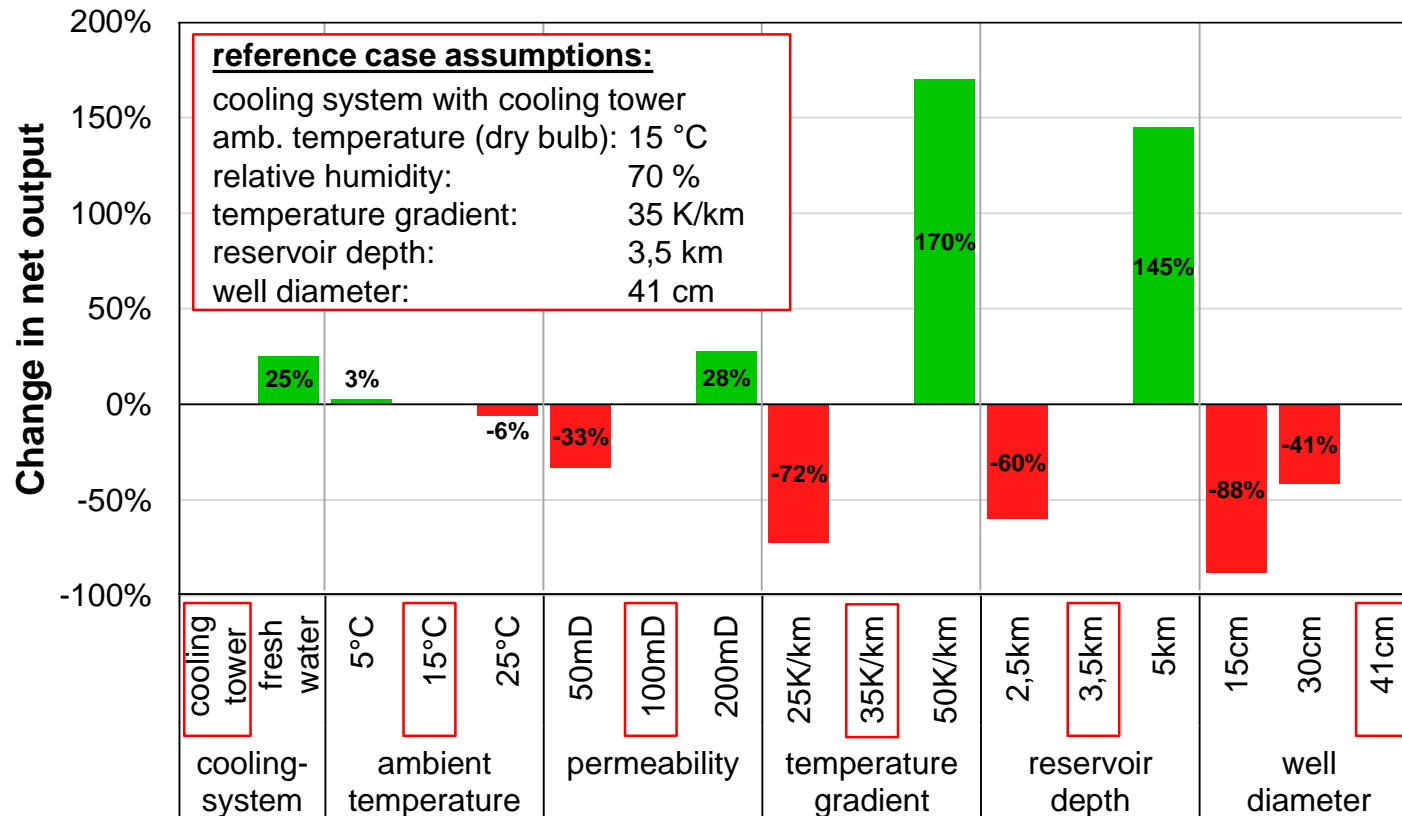
Depth	2500 m
Temp. gradient	35 K/km
Permeability-thickness product* (kh)	15.000 mD·m
injection-/ production well diameter	0,41 m

### Assumptions:

T <sub>ambient</sub>	15°C
ΔT-Pinch Condenser	7 K
ΔT-Pinch HX	5 K

**2,5-3,4 times higher net output**  
compared to brine based systems at base case

# Effects of geologic and ambient boundary conditions on net output



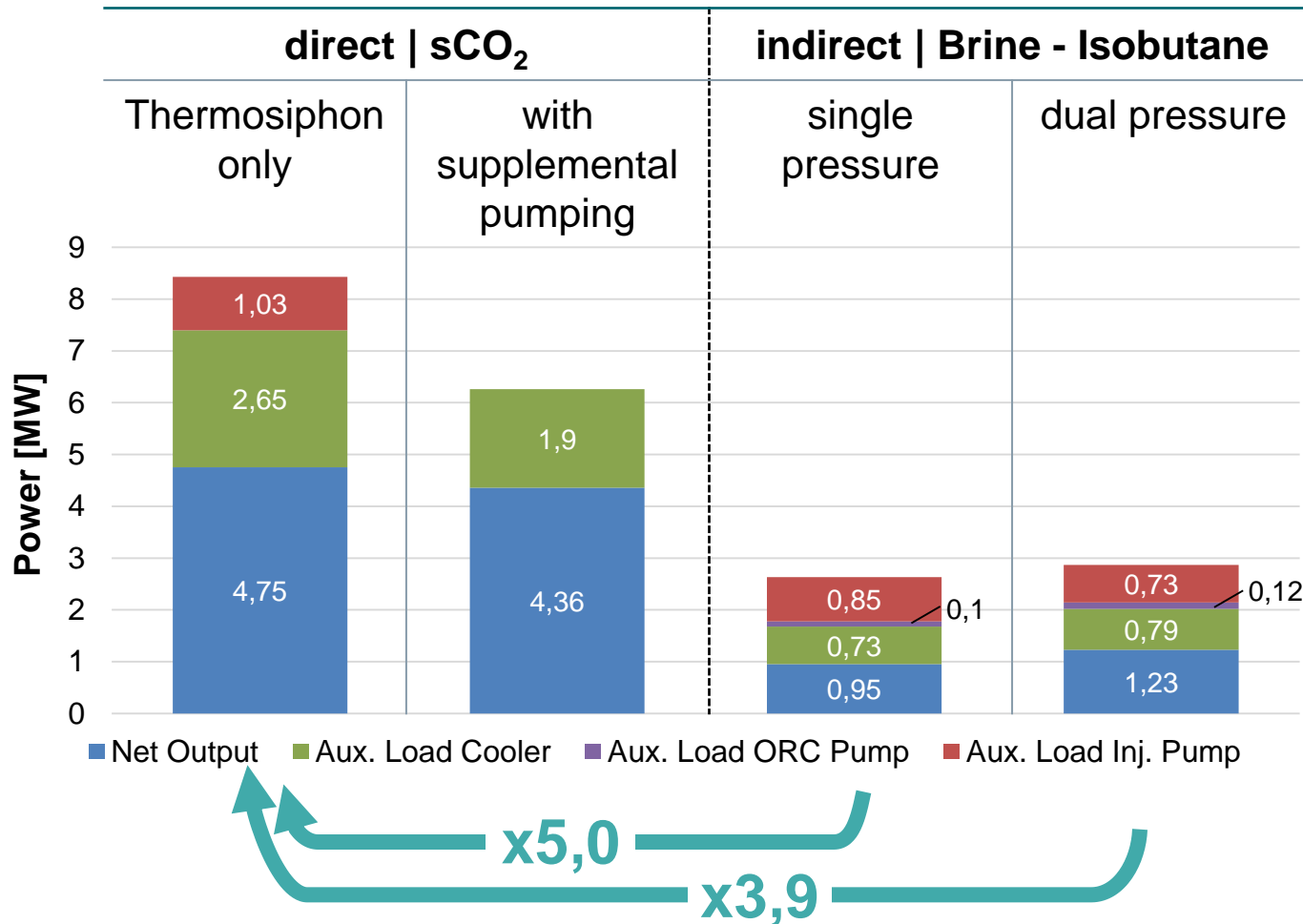
- For fresh water cooling, net power output increases due to a lower temperature of heat rejection and the elimination of auxiliary power for a mechanical draft cooling tower.
- The increase at lower ambient temperature is smaller, as the reservoir temperature also lowers.
- Regarding geological conditions, **power rises with high permeability, temperature gradient and depth**
- Large wells reduce pressure losses, the diameter must be determined depending on the permeability



# Calculation results for NGP base case optimized heat rejection



## Power Cycle Variants



### Reservoir conditions: base case

Depth	2500 m
Temp. gradient	35 K/km
Permeability-thickness product* (kh)	15.000 mD·m
injection-/production well diameter	0,41 m

### Assumptions:

T <sub>ambient</sub>	15°C
ΔT-Pinch Condenser	7 K
ΔT-Pinch HX	5 K

**3,9-5,0 times higher net output**  
compared to brine based systems at base case

# scaled geothermal cycle – wellfield pattern

## Configuration

### Number N:

equals the number of five-spot pattern on a side

**N = 1 (1x1km)**  
(five-spot pattern)

**N = 2 (2x2km)**

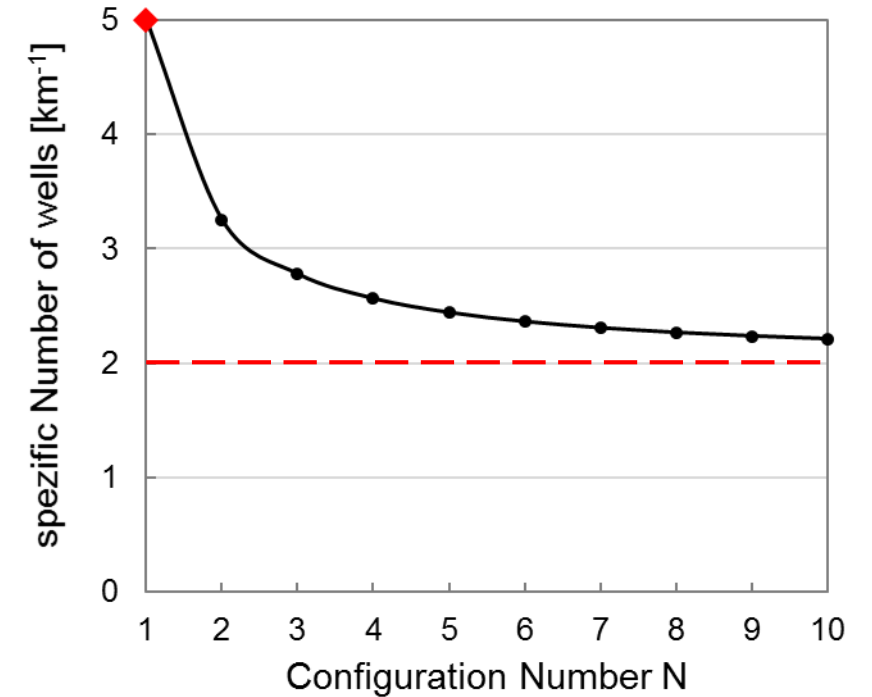
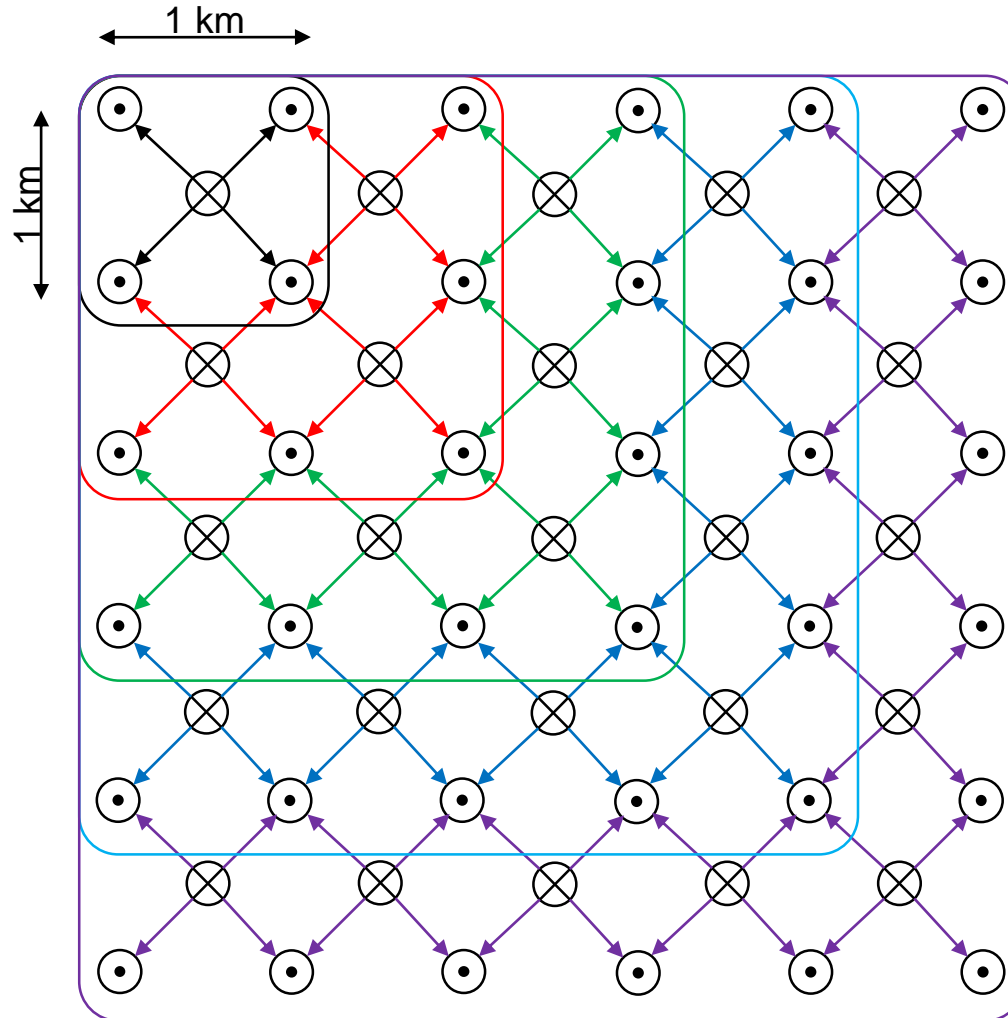
**N = 3**

**N = 4**

**N = 5**

⊙ production well

⊗ injection well



**significant savings by scaling from N = 1 to N = 2**

almost no further savings when scaling larger than N = 5

# identifying suitable locations for geothermal power plants

## 1 political framework conditions

Target region: North America (USA, Canada)  
12 of 18 large-scale CCS projects in operation in this region

## 2 reservoir analysis

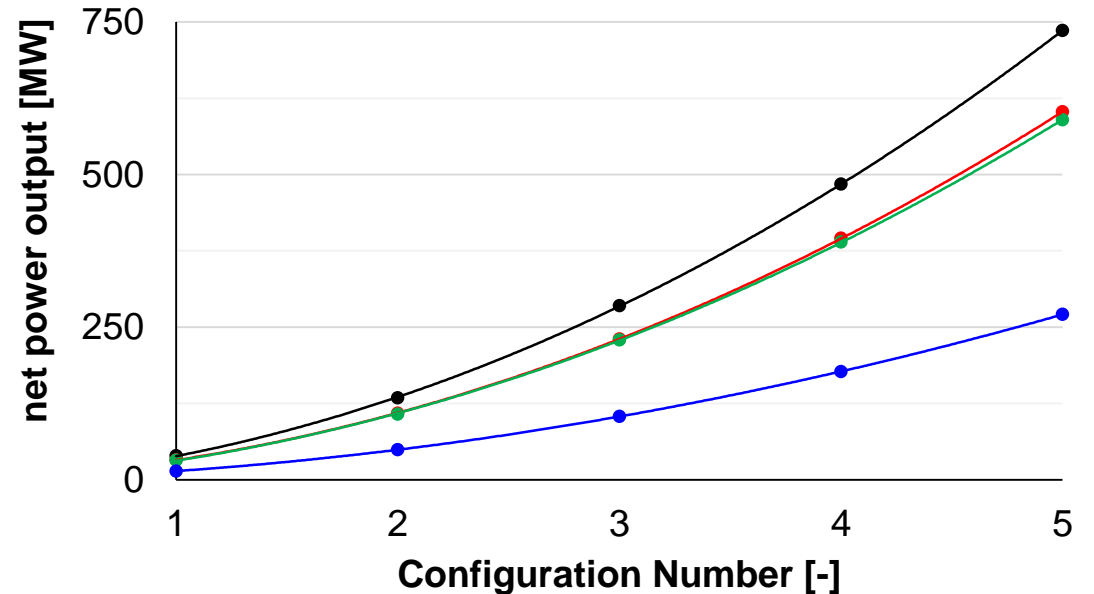
deep reservoirs, large temp. gradients, high permeability

## 3 heat rejection conditions

## 4 coverage of CO2 demand

Proximity to large, stationary CO2 emitters

## 5 population and building density



### Reservoir 1

depth: 5 km  
temp.gradient: 35 K/km  
permeability: 200 mD  
thickness: 100 m  
amb. temp.: 10 °C  
direct cooling

### Reservoir 2

depth: 3,5 km  
temp.gradient: 50 K/km  
permeability: 100 mD  
thickness: 100 m  
amb. temp.: 10 °C  
cooling tower

### Reservoir 3

depth: 5 km  
temp.gradient: 35 K/km  
permeability: 200 mD  
thickness: 100 m  
amb. temp.: 15 °C  
cooling tower

### Reservoir 4

depth: 3,5 km  
temp.gradient: 35 K/km  
permeability: 100 mD  
thickness: 200 m  
amb. temp.: 5 °C  
cooling tower

# Turbine blade path design

## 1 first approach

Siemens intermediate-pressure turbine I50-V4-M2A-60Hz

→ unfavorable pressure-to-enthalpy drop ratio

speed:  
60Hz → 30Hz



## 2 half-speed turbine

with same geometry

→ increased blading efficiency, lowered root stresses

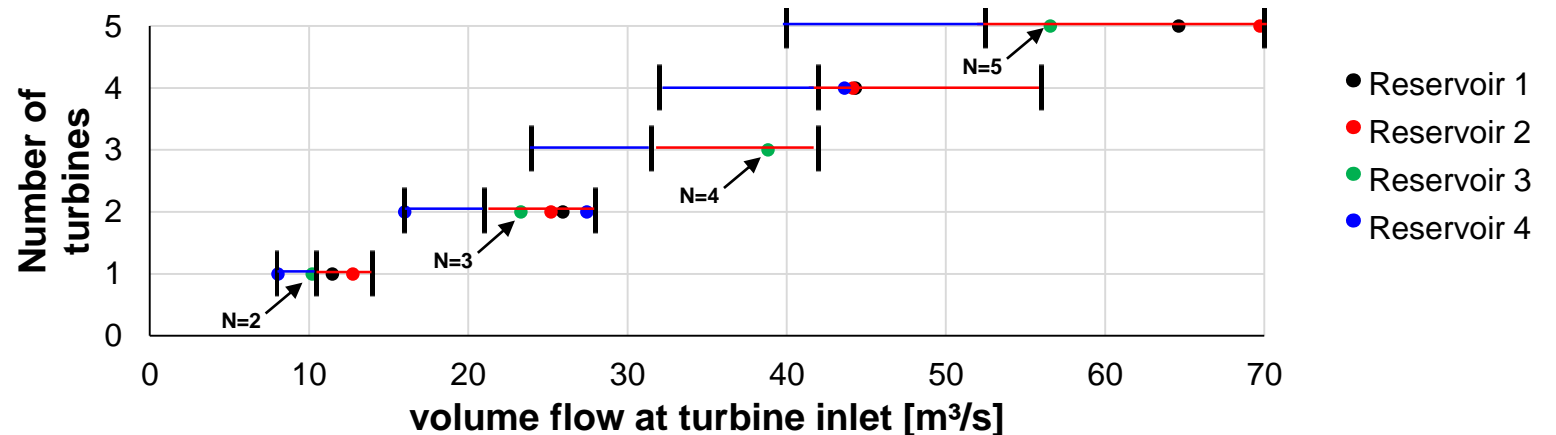
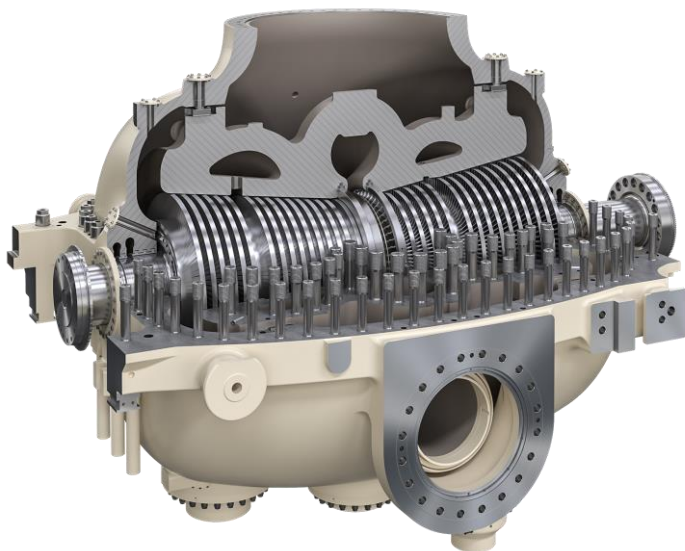
optimized geometry



## 3 CO2 turbine

geometry adjusted acc. to:  
shaft-to-tip ratio  
groove-to-shaft ratio

→ two compact designs with high efficiency and low root stresses



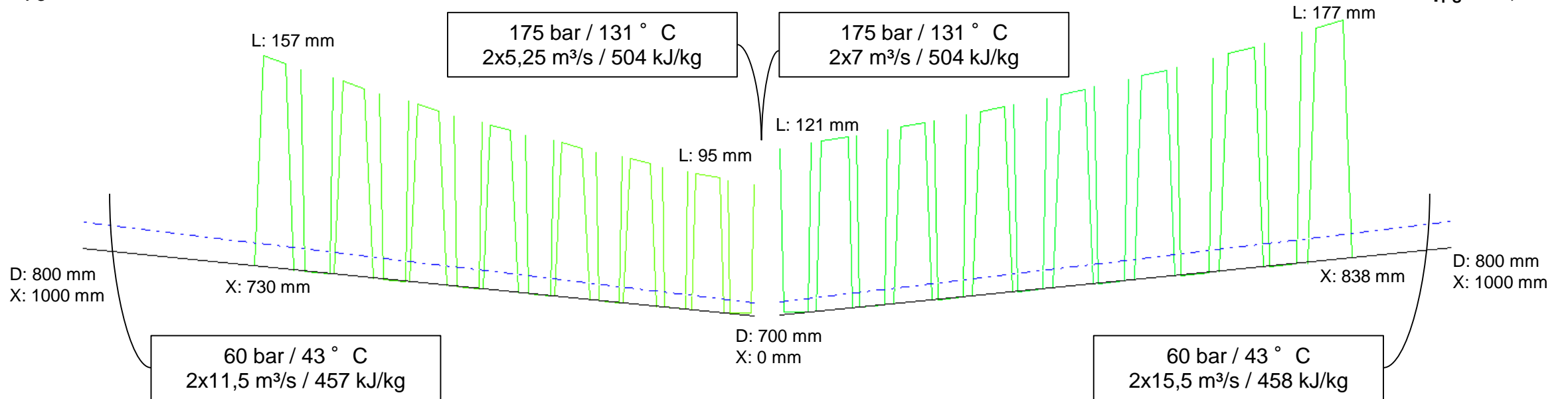
# Turbine blade path design – 150-200 MW class – 30 Hz

## minimum blading dimensions

## maximum blading dimensions

$\dot{m} = 2 \times 1650 \text{ kg/s}$   
 $P = 153 \text{ MW}$   
 $\eta_{T-S} = 94,0\%$

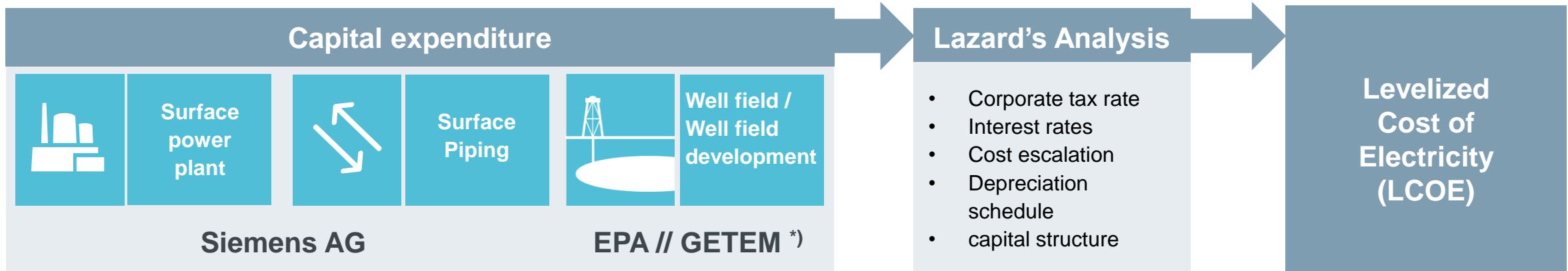
$\dot{m} = 2 \times 2225 \text{ kg/s}$   
 $P = 204 \text{ MW}$   
 $\eta_{T-S} = 93,9\%$



load coefficient  $\psi$



# Assessment of Capital expenditure and LCOE



**Surface Power Plant** → turbine train, gas cooler, pump, cooling tower, civil & small systems, electrics, engineering, project management, logistics, erection, commissioning

**Surface Piping** → pipelines between wells and surface power plant incl. raw material, fabrication, transportation, installation, engineering

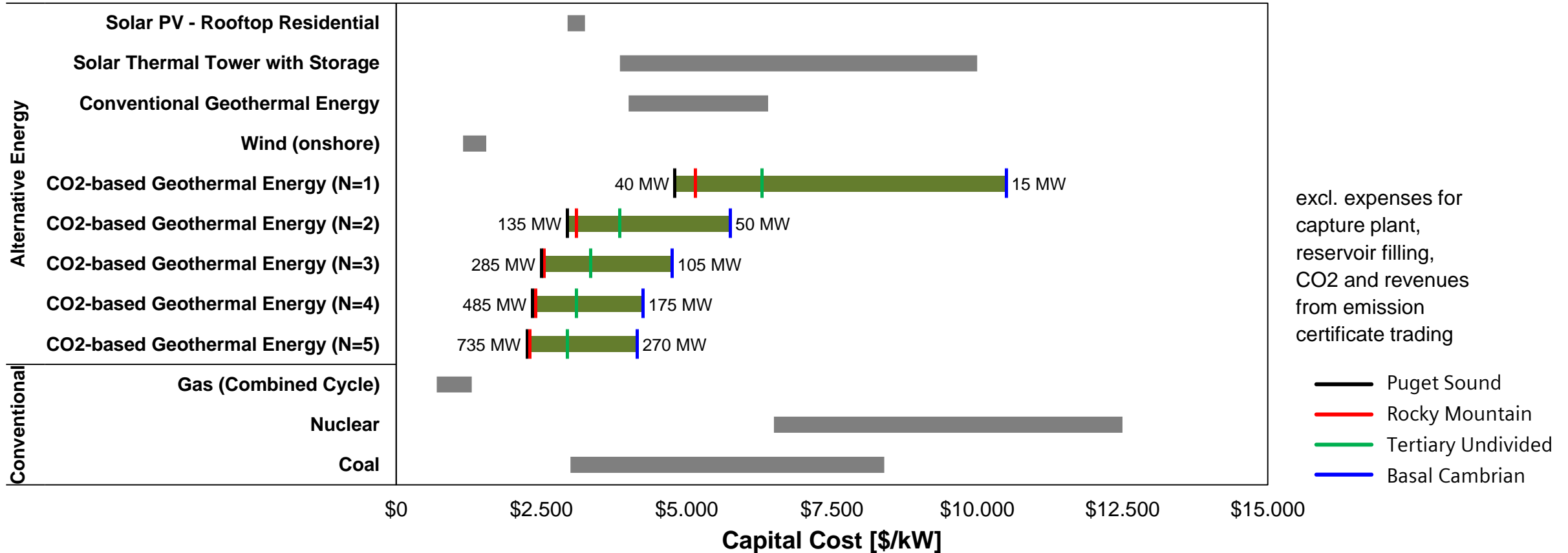
**Well field** → wells incl. drilling, corrosion protection, engineering, project management

**Well field development** → development incl. (well) monitoring equipment, stimulation, engineering, project management

$$NPV = \sum_{t=1}^n \frac{\overbrace{LCOE \cdot M_{t,el}}^{\text{Revenue}} - \overbrace{(I_t + A_t)}^{\text{Cost}}}{\underbrace{(1+i)^t}_{\text{weighted average cost of capital}}} = 0$$

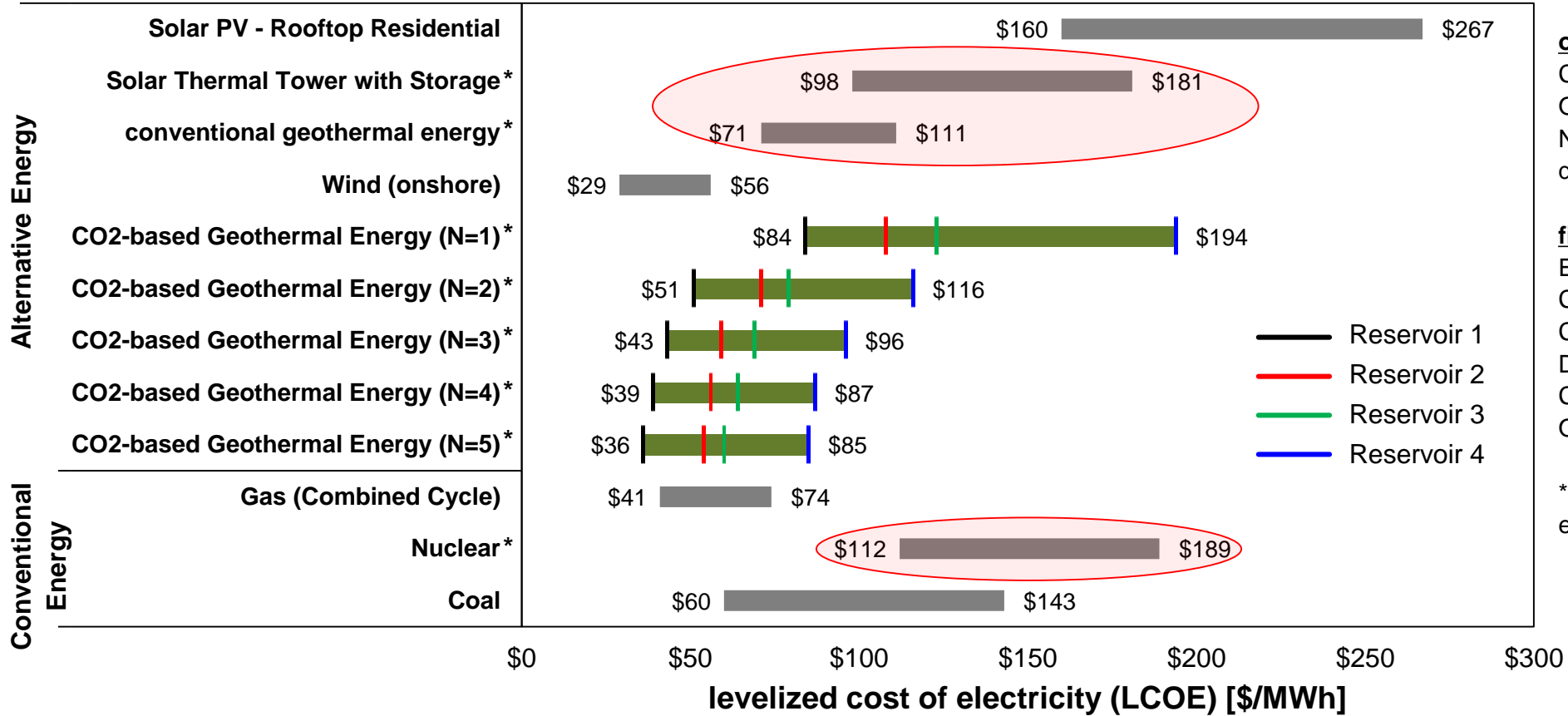
NPV: net present value,  $M_{t,el}$ : electricity produced in year t,  $I_t$ : capital expenditures in year t,  $A_t$ : annual expenses in year t, n: operation lifetime, i: interest rate

# Capital Cost - Comparison of technologies, locations and scaling



- strong dependence of capital costs on size and ambient conditions of the plant.
- absolute values are in the range of other baseload-capable and carbon-neutral plants (\*).

# LCOE - Comparison of technologies, locations and scaling



**operating conditions: \*\*)**

Capacity factor: 90 %  
 Operation lifetime: 25 years  
 No significant thermal decline during lifetime

**financial boundaries:**

Equity – Debt: 40 % - 60 %  
 Cost of Equity: 12 %  
 Cost of Debt: 8 %  
 Debt Payback Period: 25 years  
 Combined Tax Rate: 40 %  
 O&M escalation rate: 2,25 %/year

\*\*): for sCO2-based geothermal energy

- wide spread of LCOE shows the importance of a well targeted selection of the location
- results show the competitiveness of CO2-based geothermal energy, especially when scaled

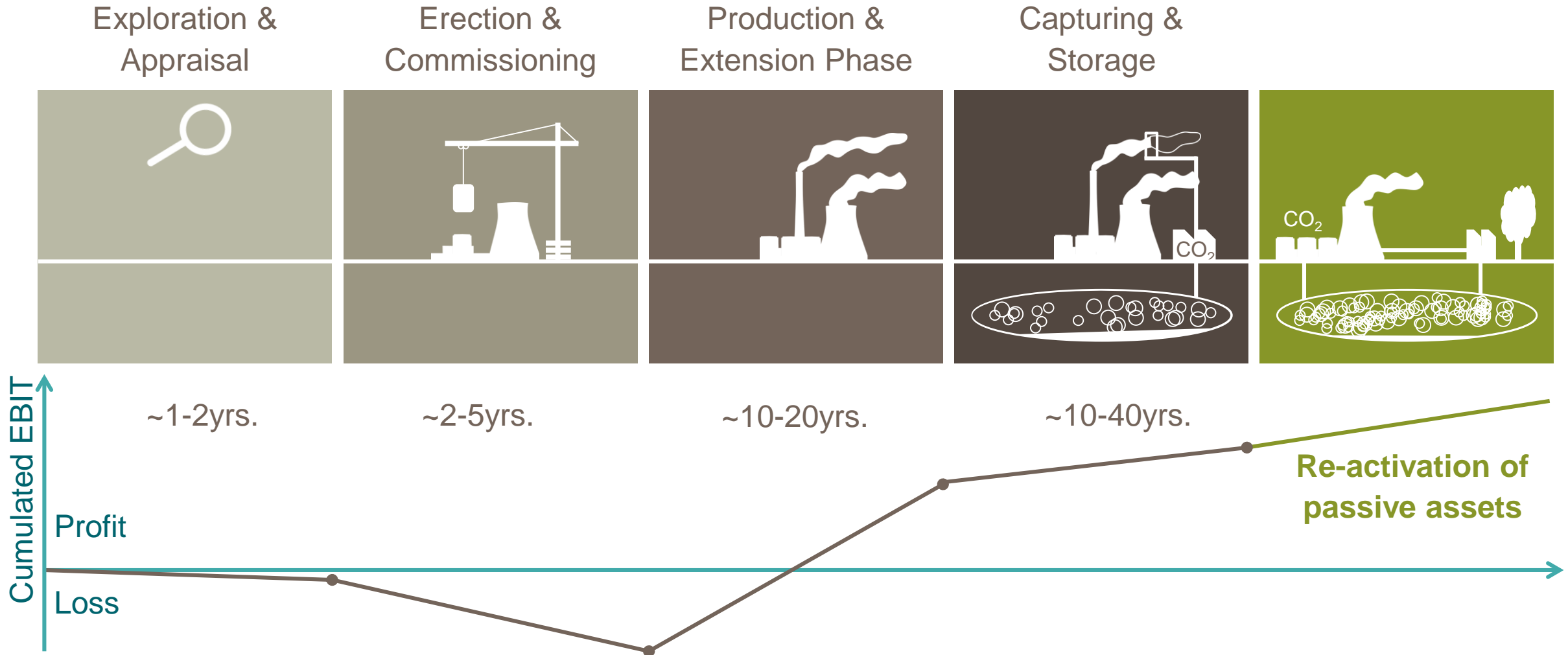


# Conclusion and Outlook

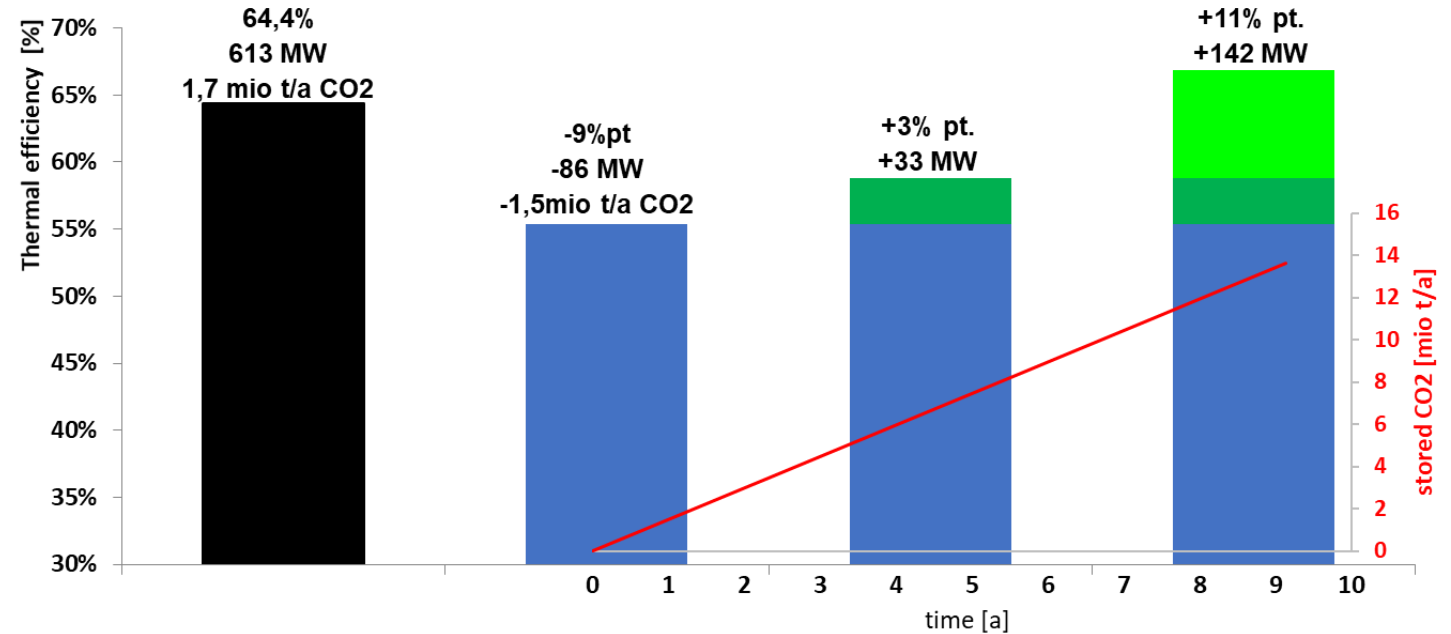
- verification of performance benefits of direct CO2 systems
  - increased power output of NGP plants by optimized heat rejection and scaling of the well pattern
  - significant reduction of LCOE
  - need for a well-targeted selection of plant site due to strongly fluctuating site-specific power output
  - competitive with other fully dispatchable and emission-free power plants
- 
- proof of concept / realization of NGP demonstrator
  - verification of the overall business case
  - realization of commercial projects

# Second Life of Combine Cycle Power Plants

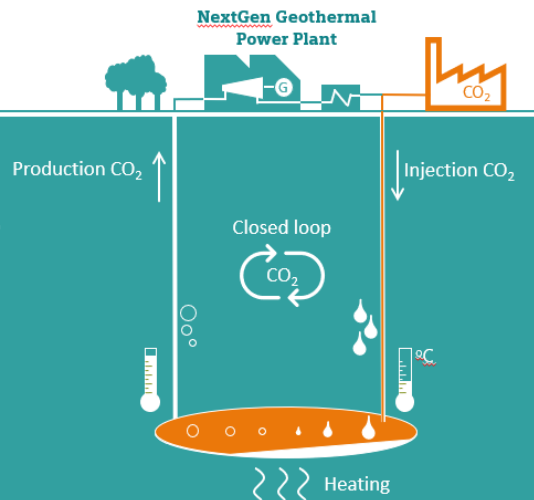
## Life Cycle Scheme of Combine Cycle Power Plants



# NGP makes CCPP emission free



## Combination of Geothermal Energy with Carbon Capture & Storage



**Combination of CCPP with CCS and NGP provides emission free power generation at highest efficiency level**

Example:  
 CCPP with SGT 9000 HL 1S  
 Reservoir data acc. to Rocky Mountain Conditions, i.e 5000 m, kxA= 10000 mDxm, 50 °C /km  
 Michael Wechsung / NextGen Geothermal Power

# Next Level Geothermal Power (NLGP)

## Life Cycle Scheme of Oil & Gas Fields & Power Plants

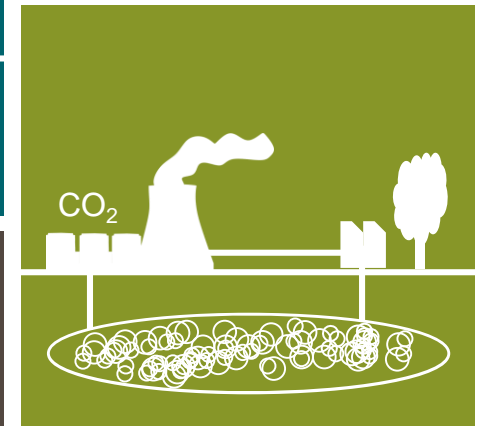
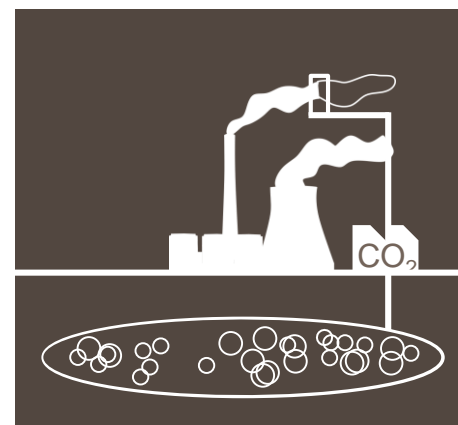
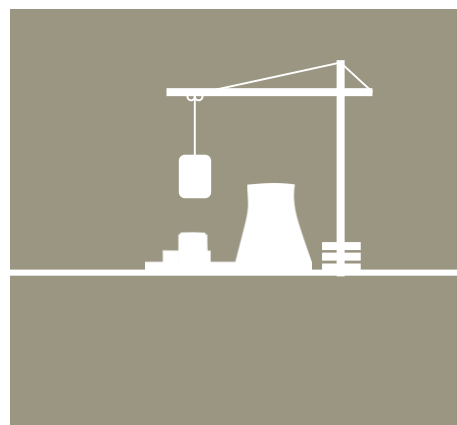
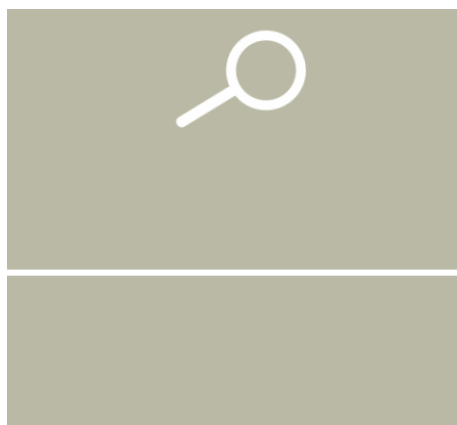
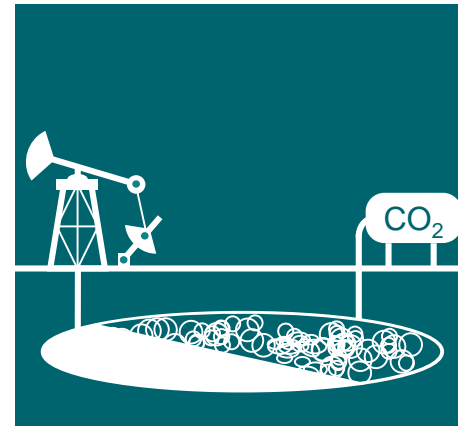
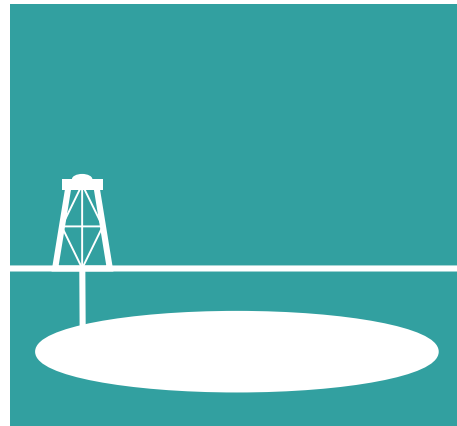


Exploration & Appraisal

Field Development

Production Phase

Enhanced O&G Recovery



**Re-activation of passive assets**



**Thank you  
for your attention.**



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