# NubiaStore: A multidisciplinary investigation for implementing CPG in the Gulf of Suez (Egypt) Mahmoud Hefny<sup>[1,2\*]</sup>, Anozie Ebigbo<sup>[1]</sup>, Chao-Zhong Qin<sup>[3,4]</sup>, Benjamin M. Adams<sup>[1]</sup>, Diya Kumbhat<sup>[1]</sup>, and Martin O. Saar<sup>[1,5]</sup>

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# **1. Introduction**

The injection of CO<sub>2</sub> into the highly permeable Nubian Sandstone of a depleted oilfield in the central Gulf of Suez basin (Egypt) can be an effective way to extract geothermal energy from deep sedimentary basins while geologically sequestering a substantial amount of CO<sub>2</sub> (main green-house gas driver), forming a so-called CO<sub>2</sub>-Plume Geothermal (CPG) system (Adams et al., 2015, Randolph and Saar (2011) and Garapati et al. (2015)). A CO<sub>2</sub> thermosiphon make CO<sub>2</sub> a favorable subsurface working fluid as will be shown next.

A schematic diagram shows the key processes on how CO2 sequestration in a saline aquifer while simulatineously producing power as in a



of the Egyptian

Finding I: The pattern of the modeled geothermal gradient map shows a higher thermal nomaly at Hammam Faraun location with 35.7 C/km geothermal gradient. The pattern is due to changes in the listric faults polarity.

### Finding II:

Nubian Sandstone (a common rock type found in the Gulf of Suez's reservoirs at depths of 2.5-4.4 km) can serve as a potential CPG subsurface convection cell. Theoretically, the CO<sub>2</sub> thermosiphon in Nubian Sandstone will increase mass flow rate, pumping-efficiency required for subsurface fluid circulation compared to water, and power production.



References

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typical CPG system



## In Gulf of Suez, where most oil/gas-producing provinces are located, suitable CPG sedimentary formations cover much of the area.

# 3. Pore-Scale Perspective

Using Synchrotron Radiation X-ray Tomographic Microscopy (SRXTM), 3D images with a voxel size of 650 nm<sup>3</sup> for Nubian Sandstone were obtained and pore network model (PNM) was construtted.

#### Finding I:

To capture the angularity of the PNM elements (where CO<sub>2</sub> will be trapped there), we found a new formulation to describe the shape factor (G) of the pore space from CT images.

$$G = \frac{R_{ins}^2}{4A_{ide}}$$

#### Finding II:

 A comparison between the experimental  $P_{c}$ - $S_{w}$  curve, measured from the MIP experiment, and drainage-main imbibition of quasi-static invasion simulation show a good agreement.

 The non-wetting phase residual saturation was determined to be ~0.35. At the residual brine saturation, the end-point relative permeability for the scCO<sub>2</sub> curve is reached at ~0.7

The van Genuchten parameters are:

- drainage: *m*=0.47[-], α=3.72e-3 [MPa] - imbibition: *m*=0.58[-], α=1.85e-3 [MPa]

# **1a. A CO<sub>2</sub> Thermosiphon Phenomena**

Since CO<sub>2</sub> density is much sensitive for pressure and temperature compared to water, the density gradients between injection-production wellbores is the main physical driver of CO<sub>2</sub> to circulate without the necessity of a mechanical pump in a so-called CO<sub>2</sub> Thermosiphoning phenomena.



The insitu thermophysics properties of CO<sub>2</sub>-brine prevail over different reservoir situations (pressure, temperature, and salinity). Their respective isoline are shown as solid grey lines. Solid black lines represent constant density ratios (0.22 - 0.85) while the dashed black lines represent constant viscosity contrasts (0.04 - 0.12). Numbered dots correspond to the investigated conditions for the current reservoir simulations



3D view of the Nubian Sandstone pore-network (domain size. 1.4x1.4x2.8 mm3). The voxel SRXTM image shows the solid phase in gray, while the extracted pore elements are overlain.



### 4. Reservoir Simulations Finding:

The behaviour of CO<sub>2</sub>-plume spread in respond to the reservoir geometry (i.e. thickness, its

compartmentalization) is shown to the right. The highest CO<sub>2</sub> concentration is found in a thin layer with a laterial confinment (from fault-seal analysis) in comparsion with

non-compartmentalized formation. In the later and due to the buoyant force, CO<sub>2</sub> tends to spread radically over a wider surface area and the concentration be a minimal at the production well.

For a Greenfield scenario, the potential net electric power generation capacity for the entire field (with a footprint of 15 km<sup>2</sup>) is 12 MWe and LCOE of <0.15 \$/kWh.

## 5. Conclusions

The high mobility of supercritical CO<sub>2</sub> results in roughly doubled geothermal heat energy extraction efficiencies, compared to water, all else being equal (such as reservoir depth and temperature). Such CO<sub>2</sub>-Plume Geothermal (CPG) power plants are particularly well suited as add-ons to (partially) depleted oil or gas reservoirs that are (or will be) used as geologic CO<sub>2</sub> sequestration formations. The electricity such add-n CPG power plants generate can then be used for the CO<sub>2</sub> capture operation and/or the CO<sub>2</sub> injection pumps/compressors and/or to can be sold to the power grid. In any case, in this way, CPG would partially or fully recover the cost of CO<sub>2</sub> Capture and Sequestration (CCS), thereby increasing the economic viability of CCS projects. In some/many locations, where geothermal temperatures are particularly high at relatively shallow depths, both CCS cost recovery and additional power sale revenues may be expected.

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